

MUDRIK, V.

MUDRIK, V.; KIRIKUTSE, I.

Total gastrectomy, resection of the lower portion of the esophagus, splenectomy, and hemipancreatectomy with subsequent anastomosis of the esophagus with the duodenum by transplanting a segment of the intestine on a pedicle. Vest.khir. no.7:122-123 J1 '57. (MIRA 10:10)

1. Iz Onkologicheskogo instituta v Bukhareste. Adres avtorov:
Bucharest 5-B, 1 Maya, D.11, Onkologicheskii institut.

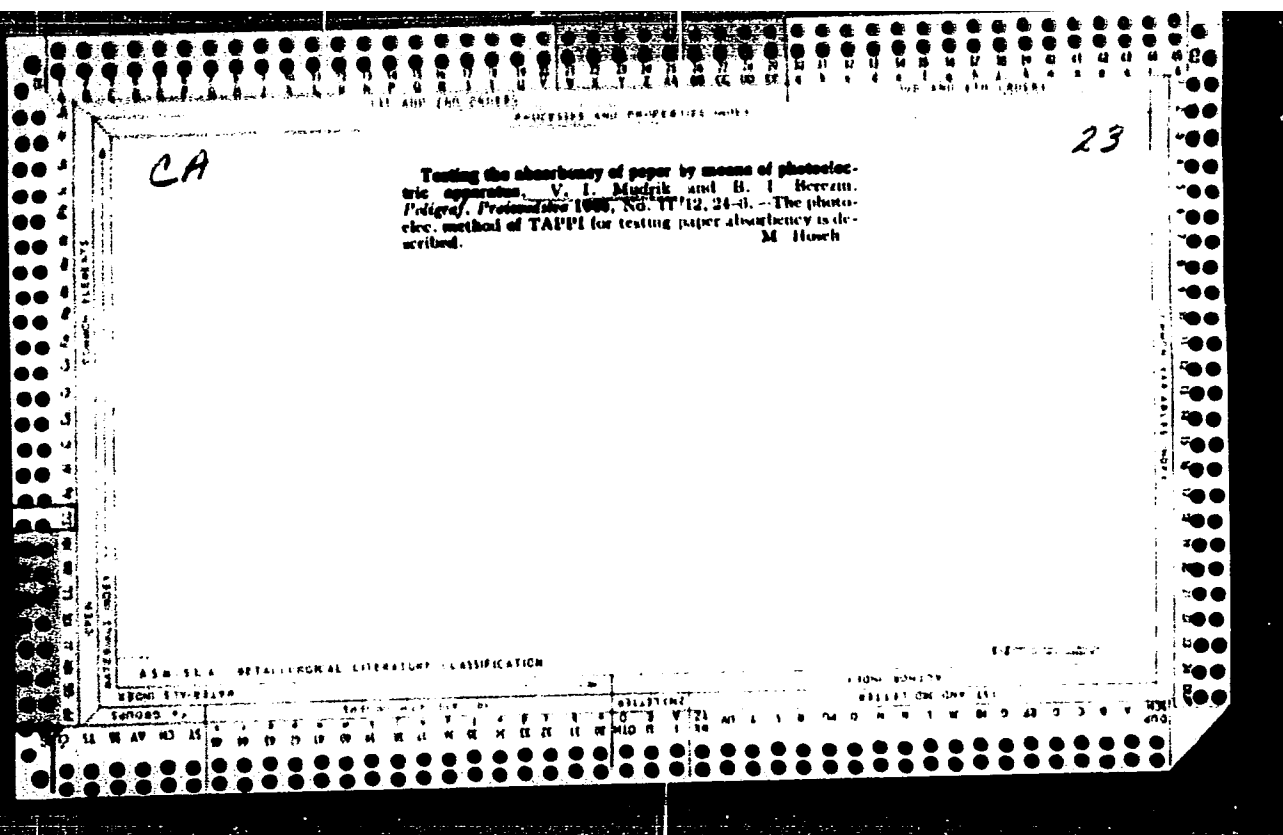
(STOMACH NEOPLASMS, surgery

total gastrectomy, partial esophagectomy, splenectomy &
hemipancreat with duodeno-esophageal anastomosis (Rus))

FELISTOVICH, N.B. (Lutsk, Volynskoy obl., L'vovskaya ul., d.82-a);
MUDRIK, V.A.; FURMANCHUK, A.A.

Invalidism due to industrial injuries of miners in the Lvov-Volyn' coal basin and measures for its decrease. Ortop., travm.
i proten. 26 no.8:57-61 Ag '65. (MIRA 18:9)

1. Iz kafedry organizatsii zdravookhraneniya i istorii meditsiny
(zav.- prof. A.A. Garash'yan) Ivano-Frankovskogo meditsinskogo
instituta (rektor - prof. G.A. Babenko) i mediko-sanitarnoy
chasti (nachal'nik - A.A. Furmanchuk) tresta "Novovolynskugol'".



MLD RIK, V.F.

8169* New Methods of Sizing Paper and Cardboard. Novye
metody prokleiki bumagi i kartona. (Russian.) V. I. Mord-
uk. *Bumazhnaia Promyshlennost'*, v. 28, no. 10, Oct. 1984, pp.
1174.
Surface sizing with zeinous, paraffinic and mixed dispersions.
Sizing in the pulp stage. Tables, diagrams. 5 ref.

MUDRIK, V.I., kandidat tekhnicheskikh nauk.

Let us be more daring in introducing continuous roll beating of
pulp. Bum.prom. 31 no.1:18-19 Ja '56. (MLDA 9;5)

1. Moskovskiy filial Giprobuma.
(Woodpulp industry)

MUDRIK, V. I.

SEMEHOVSKIY, L.A.; MUDRIK, V.I., kandidat tekhnicheskikh nauk.

Increasing the whiteness of paper. Bum.prom. 32 no.4:22-23 Ap '57.
(MLRA 10:7)

1. Glavnyy inzhener fabriki tekhnicheskikh bumag "Oktyabr'" (for Semenovskiy). 2. Moskovskiy filial Gosudarstvennogo instituta po proyektirovaniyu tsellyulozno-bumazhnoy promyshlennosti (for Mudrik).

(Paper coatings)

IVANOV, Sergey Nikolayevich. Prinimal uchastiye EYDLIN, I.Ya., kand. tekhn.nauk. MUDRIK, V.I., kand.tekhn.nauk, retsenzent; PEREKAL'SKIY, N.P., retsenzent; FLYUTE, D.M., red.; SIDEL'NIKOVA, L.A., red.isd-va; BACHURINA, A.M., tekhn.red.

[Technology of paper manufacture] Tekhnologiya bumagi. Moskva, Goslesbumizdat, 1960. 719 p. (MIRA 13:5)

1. Kafedra tsellyulozno-bumazhnogo proizvodstva Leningradskogo tekhnologicheskogo instituta (for Perekal'skiy).
(Paper industry)

MUDRIK, V., hand.tekhn.nauk

Cardboard made of reed. WFO 2 no.7:26-27 J1 '60.

(MIRA 13:7)

(Reed (Botany)) (Paperboard)

MUDRIK, V. I., kand. tekhn. nauk

Enterprises processing reed. Bum. prom. 35 no. 8:6-10 Ag '60.
(MIRA 13:8)

1. Moskovskiy filial Giprobum.
(Reed (Botany)) (Woodpulp)

MUDRIK, V.I., kand.tekhn.nauk

Plants manufacturing paperboard from waste paper. Bum.prom. 36 no.3:
14-17 Mr '61. (MIRA 14:4)

1. Moskovskiy filial Giprobuma.
(Paperboard) (Paper industry—Equipment and supplies)
(Waste paper)

SHUL'GIN, V.N.; MUDRIK, V.I.

Woodpulp and paper and paper processing industry of Cuba. Sum.
prom. 37 no.3:30-31 Mr '62. (MIRA 15:3)

1. Gosplan SSSR (for Shul'gin). 2. Moskovskiy filial Gosudarstvennogo
instituta po proyektirovaniyu predpriyatiy tsellyuloznoy i
bumazhnoy promyshlennosti (for Mudrik).
(Cuba---Paper industry)

MUDRINIC, V.



"Renewal and extension of urban electric networks in Croatia; the problem of the network of the city of Osijek."

p. 361 (Energija) Vol. 6, no. 11/12, Nov./Dec. 1957
Zagreb, Yugoslavia

SO: Monthly Index of East European Accessions (EEAI) LC. Vol. 7, no. 4,
April 1958

MUDRIY, S. P.

MUDRIY, S. P. -- "The Self-adjustment of Artificial Tooth Roots to Devices for Attaching Prostheses." Kiev Order of Labor Red Banner Med Institute imeni Acad A. A. Bogomolets, Kiev, 1956. (Dissertation for the Degree of Candidate of Medical Sciences)

SO: Knizhnaya Letopis' No 43, October 1956, Moscow

MUDROCH, O.

Electroplating in the automobile industry. p. 297.

AUTOMOBIL. (Ministerstvo automobiloveho prumyslu a zemedeliskych stroju)
Praha, Czechoslovakia, Vol. 3, No. 9, Sept. 1959.

Monthly List of East European Accessions, (EEAI), LC, Vol. 8, No. 12, Dec. 1959.
Uncl.

Z/017/60/049/007/001/003
E073/E535

AUTHOR: Mudroch, Otakar, Engineer

TITLE: Mechanization and Automation in Electroplating

PERIODICAL: Elektrotechnický obzor, 1960, Vol.49, No.7, pp.337-343

TEXT: The aim of the author was to review the present state in the field of mechanization and automation of electroplating. Primarily foreign equipment is described, i.e. an automatic straight plating line manufactured by Messrs. Deinert, Stuttgart, an automatic return line manufactured by Udyllite, Detroit, an automatic return line for bright zinc coating manufactured by F. Blasberg, Solingen-Merscheid, West Germany. As regards Czech manufactured equipment, it is stated that Kovofiniš, n.p., Ledec n. Sáz. produces two types of semi-automatic return lines with cathode ring diameters of 2 and 3.6 m. Semi-automatic equipment can be used a) in manually operated plating lines in which all the operations are in normal baths with the exception of the plating operation, and in rare cases also the degreasing operation, which is carried out in a circular or in a return bath; b) in lines in which manual operation is combined with mechanized or automated conveying. A diagrammatic sketch is

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Mechanization and Automation in Electroplating

included showing an automatic return nickel and chromating line designed by SVUOM, Prague. In conclusion it is stated that, for conditions pertaining in Czechoslovakia, mechanized straight line machines and fully automatic return machines are the most suitable. There are 9 figures and 1 Czech reference. ✓

ASSOCIATION: Automobilové závody, n.p., Mladá Boleslav
(Automobile Works, n.p. Mladá Boleslav)

SUBMITTED: January 8, 1960

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Z/032/61/011/002/004/013
E073/E235

AUTHORS: Klička, J. and Mudroch, O.

TITLE: Electrolytic Method of Removing Grinding and Polishing Pastes in Electroplating

PERIODICAL: Strojirenstvi, 1961, Vol. 11, No. 2, pp. 119- 125

TEXT: The authors have studied the efficiency of individual cleaning operations, particularly of electrolytic cleaning, for removing grinding and polishing pastes and also the influence of the operating conditions on the efficiency. They used a new test method, namely, extreme contamination of the test specimens by depositing grinding and polishing pastes by means of a spatula onto a pickled surface. A specimen of a certain surface area was first perfectly cleaned and weighed. Then, grinding and polishing paste was deposited in an extremely large quantity, which was determined gravimetrically. The most suitable method of uniform deposition of the paste was by means of a spatula onto a pickled surface. The thus contaminated specimens were then degreased in the test bath under well-defined conditions. The degree of cleanliness was determined in percentage of the original quantity of the deposited paste on the basis of the loss in weight

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determined by weighing. It was found that the layer of the deposited paste is composed of a relatively loose part (about 10% of the deposited quantity) which is usually removed in current-less alkali cleaning and a layer that adheres to the specimen and is not removed during such cleaning. Use of a pickled surface of the specimen in contrast to ground or lapped surfaces used in practical work means that the conditions of degreasing during the tests were more stringent. For determining the accuracy of the method deviation of the arithmetic mean of the quantity of deposited paste was determined for 200 specimens. It was found that the difference in the quantity of the deposited paste was not large enough to affect the reproducibility of the results during cleaning. In the experiments steel sheet specimens 1001 x 50 x 1 mm were used. These were first thoroughly cleaned and then a grinding paste containing mineral greases and oils (Paste A) or a polishing paste containing saponification greases (Paste B) was applied. The quantity of the paste on the specimens was determined gravimetrically with an accuracy of 0.1 mg. The specimens were then subjected to degreasing by immersion in an alkali bath of the type P_3HK , an

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alkaline spray bath and in an electrolytic bath. The degree of cleaning was evaluated as the percentual ratio of the drop in the weight of the paste after cleaning to the paste originally present on the specimens. It was found that the alkali immersion bath is totally unsuitable for degreasing even at 95°C and with intensive mixing. The spray bath is more favourable provided the pressure and temperature are sufficiently high and the mechanical effect of the incident liquid is strong enough. The most effective method for rough cleaning proved to be cathodic degreasing, provided it is carried out for at least 40 sec. at a temperature not less than 90°C and a current intensity of 10 A/dm². Anodic degreasing is much less effective than cathodic degreasing for the same electrolyte. For the final degreasing the anodic method is more suitable. This is due to the fact that saponification products of some of the fats and greases become concentrated; these colloidal soap particles adsorb easily on the metal surface, forming a monomolecular layer, the active part of which is orientated towards the metal, whilst the hydrophobous residue is orientated towards the solution

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and, as a result, the surface cannot be wetted. These adsorbed monomolecular layers can be removed either by long immersion in a soap-free alkali bath or by a short anodic degreasing. Consequently, the technological process of degreasing should be as follows: cathodic decreasing (rough cleaning) followed by anodic degreasing (final cleaning). The optimum conditions are the same for any bath: minimum temperature 90°C, current intensity 10 A/dm², duration of each operation at least 40 sec. The bath composition is not decisive, provided the electric conductivity is high enough and the pH is at least equal to 10. The most frequently used baths are: NaOH, Na₂CO₃, Na₃PO₄ and Na₂SiO₃. It is advantageous to use baths of the same composition for the rough and finish cleaning so as to eliminate intermediate flushing. The correctness of the laboratory results is proved by the fact that TDV, n.p., Mělník has been using over a number of years electrolytic degreasing for rough cleaning and also by the experience gained with automatic plating equipment produced by Messrs. Blasberg, West Germany and now operating at

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AZNP Mlada Boleslav. The sequence is as follows: 1) Degreasing by immersion in an alkaline bath with a concentration of 100 g/l at 98°C for 7 min. (5 sequences). 2) Degreasing by spraying with an alkaline bath of 25 g/l concentration at 60°C for 3.5 min. (3 sequences). 3) Spray flushing with water. 4) Cathodic degreasing in an alkaline bath with a concentration of 100 g/l at 60°C and a current intensity of 5 A/dm² for 70 sec. (1 sequence). 5) Anodic degreasing in a bath of equal composition at 60°C and a current intensity of 5 A/dm² for 70 sec. (1 sequence). 6) Flushing by submersion in water that has been mixed with air. The composition of the cathodic and the anodic baths was the same, namely: NaOH - 48 g/l; Na₂CO₃ - 35 g/l; Na₂SiO₃ - 15 g/l; Na₄P₂O₇ - 2 g/l; Wetting agent - 0.03 g/l. In some cases components of the paste still remained. On the basis of the results of the investigations described in this paper, the technological conditions in the automatic degreasing line was changed as follows: the temperature in the electrolytic parts of the line was increased to

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a minimum of 90°C; the current density was increased to 10 A/dm²; the cathode and anode cycles were made longer by one sequence, i.e. to a total duration of 2 min. 20 sec.; the concentration in the electrolytic bath was increased to 120-150 g/l; the spray washing with water was eliminated; the temperature of the alkali spray bath was increased to 70°C. In agreement with laboratory tests, immersion degreasing proved to eliminate only an insignificant quantity of the paste from the surface of the specimen. Degreasing by spraying proved more effective; however, due to the excessively fine atomization of the solution only about 50% of the entire paste was removed, the remainder was removed in the cathodic cycle. About 6 m² of surface could be degreased with one litre of bath liquid without affecting its activity. Then the fluid was replaced and it was found that a layer of paste residues, about 15 cm thick, collected at the bottom of the bath. This is sufficient to prove that the service life of the degreasing bath is extremely high and that the baths operate reliably even at high degrees of contamination. There are 6 figures, 1 table and 4 references: 3 Czech Card 6/7

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E073/E235

Electrolytic Method of Removing Grinding and Polishing Pastes in
Electroplating

and 1 non-Czech.

ASSOCIATION: SVÚOM, Prague (Klička) and AZNP Mladá Boleslav
(Mudroch)

✓

Card 7/7

Handwritten: RUSSIAN

15-57-7-9658

Translation from: Referativnyy zhurnal, Geologiya, 1957, Nr 7,
p 133 (USSR)

AUTHOR: Midrogina, N. S.

TITLE: Mineralization in the Formation of Some Antimony-Mercury Deposits of Central Tadzhikistan (Osobennosti protsessov mineralizatsii pri formirovani nekotorykh sur'myano-rtutnykh mestorozhdeniy Tsentral'nogo Tadzhikistana)

PERIODICAL: Materialy Vses. n.-i. geol. in-ta, 1956, Nr 10, pp 58-72.

ABSTRACT: This study dealt with localization of antimony-mercury ores in a group of deposits in Central Tadzhikistan. These deposits are located at a nonconformable contact of carbonate rock and its clastic covering silicate rock exhibiting mineral paragenesis. The study established the existence of three stages of mineralization. Each of these stages is characterized by a specific process of change of the host rock and a

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15-57-7-9658

Mineralization in the Formation of Some Antimony-Mercury (Cont.)

specific group of metals composing the ores. Alteration of the stages of mineralization was caused not only by tectonic movements but also by changes in the composition of the ore-bearing solutions. Formation of flat beds of quartzose rock occurred during the first stage of mineralization. The second period of the first stage of mineralization was preceded by local development of microbreccia in the zone of quartzose rock. Hornblende quartz with sulfides served as the cementing substance for the breccia. Metasomatic replacement of the breccia by quartz-sulfide material occurred in this same period. The main minerals of the first stage of mineralization are Fe, As, and Zn. Mineralization of the first stage occurred simultaneously with the formation of the folded structure in some sections of the deposits. The second stage of mineralization was expressed by the formation of antimonite-mercury ores. The mineralization of this stage also occurred in two periods. First quartzose-fluorite breccia was formed and quartz-filling of the limestones occurred. The processes of replacement of coarsely grained breccia by a quartzose-fluorite aggregate and of formation of metasomatic quartzose-fluorite veins played an important part in these processes. In the following period, separation of the sulfides of Sb and Hg

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MUDROGINA, N.S.

Some characteristics of the geology and mineral composition of
ores of antimony-mercury deposits and ore occurrences in the
eastern part of the Yagnob Basin. Inform.sbor.VSEGEI no.46:
79-94 '61. (MIRA 15:3)

(Yagnob Valley—Ore deposits)

MUDROGINA, N.S.; NASYBULIN, N.N.

Genesis of the silicified rocks in the Shing-Magian region.
Inform.snor.VSEGEI no.46:109-119 '61. (MIRA 15:3)
(Shing Valley--Petrology) (Magian Valley--Petrology)

MUDROGINA, N.S.; NASYBULIN, N.N.

Structural and morphological types of deposits in the
Zeravshan-Gissar antimony-mercury belt. Trudy VSEGEI 103:
145-153 *64 (MIRA 17:8)

MUDROKH, V.P.

Combined therapy of tuberculous meningitis and miliary pulmonary tuberculosis with streptomycin and PAS. Probl. tuberk., Moskva No. 1:56-58 Jan-Feb 52. (CLML 21:5)

1. Honored Physician Latvian SSR. 2. Of the Republic Anti-Tuberculosis Dispensary Latvian SSR.

MUDROKH, Ye.V., inzh.

Composition of substations without cutouts at the high-voltage end.
Elek. sta. 34 no.6:77 Jo 63. (MIRA 16:9)
(Electric substations)

25220

S/080/61/034/008/002/018
D204/D30515 2420AUTHOR: Mudrolyubova, L PTITLE: Reaction of $ZrTiO_4$ with oxides of metals of groups
II, III and IV at high temperaturesPERIODICAL: Zhurnal prikladnoy khimii, v 34, no. 8, 1961,
1679-1690

TEXT The present work is a continuation of earlier works concerned with the investigations of electrical properties and structure of $ZrTiO_4$ and its use as condenser ceramic. Its aim is to find a means of regulating the temperature coefficient of dielectric permeability of such material. For this purpose it has been necessary to find such crystalline phases which, in combination with the main component, would give mechanical mixtures or solid solutions with different Tke (temperature coefficient of dielectric permeability) but unchanged electrical properties. It was important, therefore, to determine the stability of $ZrTiO_4$ when heated with such compounds which would provide means of controlling its Tke. The compounds

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0204/0305

Reaction of $ZrTiO_4$

tested included celsian ($BaO \cdot Al_2O_3 \cdot 2SiO_2$), enorthite ($CaO \cdot Al_2O_3 \cdot 2SiO_2$), spinels ($MgO \cdot Al_2O_3$, $ZnO \cdot Al_2O_3$, $BaO \cdot Al_2O_3$, $CaO \cdot Al_2O_3$), zirconates and stannates of alkaline earth metals ($BaZrO_3$, $CaZrO_3$, $BaSrO_3$, $CaSrO_3$, $MgSnO_3$), $MgTiO_3$ (i.e. compounds exhibiting a complexing $BaZrO_3$) positive TKe, and also a series of oxides (CaO , CrO , BaO , BeO). All these compounds were synthesized at 1200-1300°C and their composition confirmed by x-ray analysis. Further investigations involved the following systems: 1) $ZrTiO_4$ - $BaO \cdot Al_2O_3 \cdot 2SiO_2$; 2) $ZrTiO_4$ - $CaO \cdot Al_2O_3 \cdot 2SiO_2$; 3) $ZrTiO_4$ - $MgO \cdot Al_2O_3$; 4) $ZrTiO_4$ - $ZnO \cdot Al_2O_3$; 5) $ZrTiO_4$ - $BaO \cdot Al_2O_3$; 6) $ZrTiO_4$ - $CaO \cdot 6Al_2O_3$; 7) $ZrTiO_4$ - $BaZrO_3$; 8) $ZrTiO_4$ - $CaZrO_3$; 9) $ZrTiO_4$ - $BaSrO_3$; 10) $ZrTiO_4$ - $CaSrO_3$; 11) $ZrTiO_4$ - $MgSnO_3$; 12) $ZrTiO_4$ - $MgTiO_3$; 13) $ZrTiO_4$ - CaO ; 14) $ZrTiO_4$ - CrO ; 15) $ZrTiO_4$ - BaO ; 16) $ZrTiO_4$ - BeO . Out of the sixteen compounds only celsian, enorthite, ganite, magnesium titanate and beryllium oxide did not react with $ZrTiO_4$. All other decomposed with the separation of monoclinic or cubic ZrO_2 . Only the men-

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Reaction of $ZrTiO_4$

tioned five, therefore, could be used for further investigations. (Table 12). The TKe of enorthite is considerably higher than that of $ZrTiO_4$ and even small additions of the former displace the TKe of the mixture toward more positive values. Dielectric losses for the $ZrTiO_4 - CaO \cdot Al_2O_3 \cdot 2SiO_2$ system are smaller than those for $ZrTiO_4 - BaO \cdot Al_2O_3 \cdot 2SiO_2$ although $CaO \cdot Al_2O_3 \cdot 2SiO_2$ system has low tan values (tangent of an angle of dielectric losses). Additions of 15% anorthite practically do not affect the sintering temperature of the sample. Dielectric permeability and TKe of samples with increase $ZnO \cdot Al_2O_3$ concentration vary according to the laws of mechanical mixtures. Dielectric losses under normal conditions are practically equal within the whole range of concentrations, but the temperature coefficient of tan decreases with the increased concentration of ganite. When investigating $ZrTiO_4 - MgTiO_3$ system only 10% $MgTiO_3$ concentrations were considered since no sintering occurred with more than 10% of $MgTiO_3$. For $ZrTiO_4 - BeO$ system the sintering temperature corresponded to 1500°C for 2 - 10% BeO and about 1400 - 1450°C for 10 - 20% dielectric permeability of

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Reaction of $ZrTiO_4$...

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$ZrTiO_4$ changes only slightly with the increase BeO content and the absolute T_{KE} decreases. For the purpose of fuller characterization of the investigated systems changes of resistances of the insulating specimens were studied at temperatures of 300 - 400°C and 1000 V/mm. The results of testing are represented in Fig. 8. The mechanism of $ZnO \cdot Al_2O_3$ synthesis and its refractory properties were studied by Maynarskiy and Sidorov and according to their results the synthesis of ganite is most efficient at 1200°C using crude alumina. The authors of the present work were unable, however, to obtain sintered samples from crude alumina, and used alumina roasted at 1350°C and synthesized ganite at 1250°C. Furthermore, it was established that the electrical properties of $ZrTiO_4 \cdot ZnO \cdot Al_2O_3$ system are independent of the method of preparing $ZrTiO_4$ which could be added to the system as a ready made compound or synthesized in situ from ZrO_2 and TiO_2 . As ganite decomposes in reducing medium, it has been necessary to examine the effect of various gaseous media on sintering and the electrical properties of ceramics containing 25% ganite. For this purpose the samples were heated for 2 hours at 1450°C in

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Reaction of $ZrTiO_4$...

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atmospheres of gas mixtures. It has been established that the sintering of granite-containing systems may be carried out in oxidizing or neutral medium. There are 19 tables, 8 figures and 10 references: 8 Soviet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: Frank, Brown, Dywez, J. Am. Cer. Soc. 37, 129, (1954); L.W. Coughanour, R.S. Roth, V.A. De-Prose, J. Res. National Bureau of Standards, 52, 1, (1954).

SUBMITTED: October 15, 1960

ТАБЛИЦА 12

Table 12 Legend: a)

Material: 1 - zirconium titanate, 2 - cel-esin, 3 - anorthite, 4 - granite, 5 - magnesium titanate. b) Chemical formula; c) Sintering temperature.

Материал	Химическая формула	Температура спекания (°C)	α	TK · 10°	Δnδ · 10°
1. Титанат циркония [1]	$ZrTiO_4$	1700—1750	39	-110	2—3
2. Целезин	$BaO \cdot Al_2O_3 \cdot 2SiO_2$	1350	6	+ 60	2—3
3. Анортит	$CaO \cdot Al_2O_3 \cdot 2SiO_2$	1350	6	+400	2—3
4. Гранит	$ZnO \cdot Al_2O_3$	1500	10	+120	3—5
5. Титанат магния [5]	$MgTiO_3$	1450	13	+ 70	2—3

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MUDROLYUBOVA, L. P.

Dissertation defended for the degree of Candidate of Technical Sciences
at the Institute of Silicate Chemistry imeni I. V. Grenbenshchikov in 1962:

"Investigation of Ceramic Dielectrics Based on the System ZrO_2-TiO_2 ."

Vest. Akad. Nauk SSSR. No. 4, Moscow, 1963, pages 119-145

BOGORODITSKIY, Nikolay Petrovich; KAL'MENS, Natan Vladimirovich;
NEYMAN, Moisey Isakovich; POLYAKOVA, Natal'ya
Lavrent'yevna; ROTENBERG, Boris Abovich; SALITRA,
Dmitriy Borisovich; AFANAS'YEVA, Margarita Aleksandrovna;
FRIDBERG, Illariy Dmitriyevich; Prinimala uchastiye
MUDROLYUBOVA, L.P.; PASYNKOV, V.V., red.; ZHITNIKOVA, O.S.,
tekhn. red.

[Ceramic materials in radio engineering] Radiokeramika. Mo-
skva, Gosenergoizdat, 1963. 553 p. (MIRA 16:12)
(Radio--Equipment and supplies)
(Electric engineering--Materials)
(Ceramic materials)

MUDNOV, A.I.

Initiative of the greatest importance. Izv.vys.ucheb.zav.; tekhn.tekst.
prom. no.1:157-159 '63. (MIRA 16:4)

1. Ivanovskiy tekstil'nyy institut imeni M.V.Frunze.
(Textile industry) (Efficiency, Industrial)

MUDROV, A.M.

Facies and formation of coal sediments of the Podgorodnoye
deposit in southern Maritime Territory. Trudy Lab. geol. ugl.
no.10:201-219 '60. (MIRA 13:9)
(Murav'yev-Amurskiy Range—Coal geology)

VOLKOVA, I.B.; NALIVKIN, D.V.; SLATVINSKAYA, Ye.A.; BOGOMAZOV, V.M.;
 GAVRILOVA, O.I.; GUREVICH, A.B.; MUDROV, A.M.; NIKOL'SKIY, V.M.;
 OSHURKOVA, M.V.; PETRENKO, A.A.; POGREBITSKIY, Ye.O.; RITENBERG,
 M.I.; BOCHKOVSKIY, F.A.; KIM, N.G.; LUSHCHIKHIN, G.M.; LYUBER,
 A.A.; MAKEDONTSOV, A.V.; SENDERZON, E.M.; SINITSYN, V.M.; SHORIN,
 V.P.; BELYANKIN, L.F.; VAL'TS, I.E.; VLASOV, V.M.; ISHINA, T.A.;
 KONIVETS, V.I.; MARKOVICH, Ye.M.; MOKRINSKIY, V.V.; PROSVIRYAKOVA,
 Z.P.; RADCHENKO, O.A.; SEMERIKOV, A.A.; FADDEYEVA, Z.I.; BUTOVA,
 Ye.P.; VERBITSKAYA, Z.I.; DZENS-LITOVSKAYA, O.A.; DUBAR', G.P.;
 IVANOV, N.V.; KARPOV, N.F.; KOLESNIKOV, Ch.M.; NEFED'YEV, L.P.;
 POPOV, G.G.; SHTEMPER', B.M.; KIRYUKOV, V.V.; LAVROV, V.V.;
 SAL'NIKOV, B.A.; MONAKHOVA, L.P.[deceased]; MURATOV, M.V.;
 GORSKIY, I.I., glav. red.; GUSEV, A.I., red.; MOLCHANOV, I.I.,
 red.; TYZHNOV, A.V., red.; SHABAROV, N.V., red.; YAVORSKIY, V.I.,
 red.; REYKHERT, L.A., red.izd-va; ZAMARAYEVA, R.A., tekhn. red

[Atlas of maps of coal deposits of the U.S.S.R.] Atlas kart ugle-
 nakopleniya na territorii SSSR. Glav. red. I.I.Gorskiy. Zam.
 glav. red. V.V.Mokrinskiy. Chleny red. kollegii: F.A.Bochkovskiy
 i dr. Moskva, Izd-vo Akad. nauk SSSR, 1962. 17 p.

(MIRA 16:3)

1. Akademiya nauk SSSR. Laboratoriya geologii uglia. 2. Chlen-
 korrespondent Akademii nauk SSSR (for Muratov).

(Coal geology—Maps)

MUDROV, I. I.

Materialovedenie dlia stoliarov [Knowledge of materials for carpenters]. Izd. 2-e, Moskva, Trudizervizdat, 1952. 128 p.

SO: Monthly List of Russian Acquisitions, Vol 6 No 4, July 1953

MIRONOV, S.A., professor, doktor tekhnicheskikh nauk, STOL'NIKOV, V.V.,
doktor tekhnicheskikh nauk [reviewers]; SKRAMTAYEV, B.G., POPOV, N.A.,
GERLIVANOV, N.A., MUDROV, G.G. [authors].

"Building materials." B.G.Skrantaev, N.A.Popov, N.A.Gerlivanov,
G.G.Mudrov. Reviewed by S.A.Mironov, V.V.Stelnikov. Stroi.prom. 31
no.11:47-48 N '53. (MLRA 6:12)
(Building materials) (Skrantaev, B.G.) (Popov, N.A.)

MUDROV, G.G.

The Committee on Stalin Prizes (of the Council of Ministers USSR) in the fields of science and inventions announces that the following scientific works, popular scientific books, and textbooks have been submitted for competition for Stalin Prizes for the years 1952 and 1953. (Sovetskaya Kultura, Moscow, No. 22-40, 20 Feb - 3 Apr 1954)

<u>Name</u>	<u>Title of Work</u>	<u>Nominated by</u>
Skrantayev, B.G.	"Construction Materials"	Moscow Construction Engineer-
Popov, N.A.	(textbook, 5th edition)	ing Institute imeni V.V.
Gerlivanov, N.A.		Kuybyshev
<u>Mudrov, G.G.</u>		

RC: W-30604, 7 July 1954

MUDROV, G.G., kandidat tekhnicheskikh nauk.

Designating the coefficient of homogeneity of pavement
concrete. Avt. dor. 19 no.6:24-25 Je '56.

(MLRA 9:9)

(Pavements, Concrete)

MUDROV, G.G., dotsent, kandidat tekhnicheskikh nauk.

Metal forms for taking concrete samples. Avt. dor. 19 no.10:
17-18 0 '56. (MLRA 9:12)

(Concrete--Testing)

679L7

15.3200

S/097/59/000/07/012/021

E141/E164

AUTHORS: Mudrov, G.G. (Cand.Tech.Sci.), and
Mikhaylov, A.V. (Cand.Tech.Sci.)

TITLE: Heat-Resistance of Concrete Runways of Airfields³

PERIODICAL: Beton i zhelezobeton, 1959, Nr 7, pp 318-320 (USSR)

ABSTRACT: Concrete runways of airfields are subjected to high temperatures caused by modern types of aircraft. The surface of the runway breaks in those parts where the heat is most frequent. It is therefore necessary to look into the problem of materials and technology used for such runways. This article describes results of tests of ordinary Portland-cement concrete subjected to heat caused by exhaust gases, of its heat resistance and frost resistance; and recommendations are made to achieve improvements. First of all the fire resistance of ordinary concrete is evaluated. If concrete is heated up to 250 °C for a long period dangerous structural changes do not appear, though its strength is partly reduced. At higher temperatures than 250 °C the strength is considerably impaired. High temperatures of long duration are not frequent; normal conditions are the short-time

Card
1/4

67947

S/097/59/000/07/012/021
E141/E164

Heat-Resistance of Concrete Runways of Airfields

effect of exhaust gases. Tests were carried out in heating ordinary concrete slabs 4 X 5 m in size, 40 cm thick. Temperatures were measured along the depth of the slab and of the ground below, using thermocouples situated as shown in Fig 1. The temperatures were measured by means of an automatic "electronic bridge". The heating times were 5, 10, 15, 20, and 30 minutes. The surface face temperature reached 200-400 °C. The temperature variation according to the depth of the slab and the time is shown in Fig 2, and the distribution of maximal temperature according to the cross-sectional depth of the slab is given in Table 1. The tests showed that: the process of warming up affects the whole thickness of the concrete but practically does not affect the temperature of the underlying ground; change of temperature in the slab takes place relatively slowly, a considerable drop in temperature takes place through the thickness of concrete slab; the absolute value of the

Card
2/4

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S/097/59/000/07/012/021

E141/E164

Heat-Resistance of Concrete Runways of Airfields

temperature of the core of the concrete is within the limits allowed for ordinary Portland-cement concrete. Investigations also showed that the speed at which the temperature is conveyed by the ground in the initial period of warming up of the slab is low. Fig 3 shows how the temperature drops along the cross-section of concrete slab. Calculations show that concrete subjected to heat for a longer period than 5 minutes may crack due to thermal deformation. It was found that the heating of the concrete caused flaking 3 to 15 cm in size and 1 to 2 cm thick, and that the weaker the concrete the more numerous the flakes. To increase heat-resistance of slabs of ordinary concrete it is necessary to increase the strength of the top layer of concrete. A simple and satisfactory way is the use of absorbent materials applied to the top of the slabs immediately after they are cast. Such materials are, for example, ordinary building board, paper and wrapping paper. The surface of the concrete covered by paper differs considerably from that which is not covered up. When the covered concrete was subjected

Card
3/4

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S/097/59/000/07/012/021

E141/E164

Heat-Resistance of Concrete Runways of Airfields

to the maximal temperature of 600 °C for 30 minutes no visible deterioration occurred. Ordinary concrete slab subjected to this temperature showed visible deterioration. Test cubes protected by paper showed strength in tension 18% higher than ordinary samples. Tests were also carried out in regard to frost-resistance of ordinary concrete subjected to high temperatures. Granite and limestone coarse aggregate was used for the concrete. Test cubes for this investigation 15 X 15 X 55 cm were cured under normal conditions for 28 days. First the test cubes were subjected to repeated heating up to 600 °C and then to repeated freezing and de-freezing. The values obtained in these tests are given in Table 2. It was found that after repeated heating and freezing the strength in bending of the concrete based on granite aggregate was considerably lower, whereas concrete based on limestone aggregate retained its strength.

There are 3 figures and 2 tables.

Card
4/4

MUDROV, Gennadiy Illarionovich; MARKELOV, Georgiy Dmitriyevich;
GLADKOV, V.A., red.; SYCHEVA, V.A., tekhn. red.

[Shock workers at building sites] Udamniki stroitel'nykh
ploshchadok. Murmansk, Murmanskoe knizhnoe izd-vo, 1961.
13 p. (MIRA 16:6)

(Murmansk--Building)

MUDROV, KH.

MUDROV, KH. Improving the quality of the raw hides, paramount economic task. p. 13.

Vol. 5, No. 5, 1956.
LEKA PROMISHLENOST.
TECHNOLOGY
Sofia, Bulgaria

So: East European Accession, Vol. 6, No. 3, March 1957

MUDROV, Khristo

Effect of estrogens and prolan on hen egg productivity. Selskostep
nauka 2 no.8:1000-1007 '63

VOROB'YEV, S.V.; VOLKOVEDOV, P.S., kandidat tekhnicheskikh nauk; MUDROV, N.A.,
inzhener.

Producing profiles of various cross-sections by forging with shaped forging blocks. Vest.mash. 33 no.3:28-32 Mr '53.

(MLRA 6:5)
(Forging)

158350 also 1372

26867
S/080/61/034/004/008/012
A057/A129

AUTHORS: Shtraykhan, G. A., Al'shits, I. M., Meshcheryakow, V.V., Mudrov,
O. A., Levitakaya, O. M.,

TITLE: Copolymers of the polyesters of maleic and methacrylic acid - a
new type of binder for glass-reinforced plastics

PERIODICAL: Zhurnal prikladnoy khimii, v. 34, no. 4, 1961, 888 - 894

TEXT: A method for the preparation of a new type (MA-3 [MA-3]) of unsaturated polyester resins is described. The resins are solutions of maleate polyesters in polyesters of methacrylic acid, which are copolymerized by adding some initiator hardener mixtures. The resulting MA-3 polyester does not contain volatile monomers (such as styrene, methylmethacrylate etc.). Hence more hygienic work conditions were attained by using MA-3 polyester resin as binder for glass-reinforced plastics. The latter have better mechanical properties than glass-reinforced plastics based on MH-1 (PN-1) maleate polyester resin or 911-MC (911-PS) acrylate polyester binder. An improvement of technology is also attained since MA-3 resin has a longer gelatination time. Unsaturated resins called acrylate polyester resins were developed in the USSR by A. A. Berlin et al. (Ref. 6:

X

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26867

3/080/61/034/004/008/012

A057/A129

Copolymers of the polyesters of maleic

Vysokomol. soyed., 1,7, 951, 1959; Ref. 7: Vysokomol. soyed., 1,7, 957, 1959). These resins are products of the polycondensation of glycols and glycerine with dibasic saturated acids (phthalic or sebacic acid) and monobasic methacrylic acid. The introduction of a monobasic unsaturated acid makes possible regulation of the chain growth in the polyesterification process and thus manufacture of acrylate polyesters with a different degree of polymerization. According to Ya. D. Avrasin and A. I. Prigoreva (Ref. 8: Plast. massy, 1, 13, 1960) properties of glass-reinforced plastics based on acrylate polyesters are caused by the functional force and distance between the unsaturated acrylic end-radicals in the polyester chain. Another common polyester resin is the maleate polyester resin described by P. Z. Li et al. (Ref. 5: Plasticheskiye massy, 2, 19, 1959). A drawback of the manufacture of both types, acrylate and maleate polyesters is evolution of styrene vapors which produce a highly poisoned atmosphere. For this reason in the present work the production of polyester resins not containing volatile poisonous compounds and having good physical and mechanical properties was investigated. Preparation of copolymers of maleate polyesters and low molecular acrylate polyesters with the ability to be solvent and copolymerization component, according to a patent of the present authors (Ref. 9: Soviet patent no. 132819,

Card 2/8

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S/080/61/034/004/008/012

A057/A129

Copolymers of the polyesters of maleic

ACTT(δ)C₂ (ASTT (b)S₂) satin 8/3 with and without removal of the lubricant) with the manufactured MA-3 resin, 5 and 10 mm thick sheets were formed and tested 25 days after preparation. The results are presented in Table 6, showing several advantages in relation to the PN-1 resin and 911-MS binder. Investigations carried out by Yu. A. Agashin, M. M. Tuchenko and P. V. Sidyakov in the Institut gigiyeny truda i proffzabolevaniy (Institute of Industrial Hygiene and Occupational Diseases) demonstrated the advantage of using MA-3 resin instead of PN-1 resin considering sanitary conditions, since the total amount of styrene formed during hardening of PN-1 resin is 12 times greater than for MA-3 resin. There are 4 figures, 6 tables and 9 references: 6 Soviet-bloc and 3 non-Soviet-bloc. The two references to the English-language publications read as follows: Johan Bjorksten. Polyesters and their applications., N. Y., 1956; Phillip Morgan, Glass Reinforced Plastics, London, 1957.

SUBMITTED: August 4, 1960

Card 4/8

a

ACCESSION NR: AP4043318

S/0191/64/000/008/0011/0012

AUTHOR: Al'shits, I. M.; Gladkaya, L. A.; Grad, N. M.; Mudrov, O. A.

TITLE: Study of self-extinguishing polyester resins

SOURCE: Plasticheskiye massy*, no. 8, 1964, 11-12

TOPIC TAGS: resin, polyester resin, self extinguishing polyester resin, modified resin, glass reinforced plastic, self extinguishing reinforced plastic

ABSTRACT: Self-extinguishing polyester resins for heat-resistant glass-reinforced plastics have been developed by the modification of combustible polyester resins. Self-extinguishing resins were prepared from PN-1, PN-3, MA-3, and NPS-609-21 Soviet industrial polyester resins by the addition of chlorine-containing compounds and antimony trioxide. The settling of these additives was prevented by the incorporation into the resin of the U-333 light-colored filler. The properties of the uncured and cured self-extinguishing polyester resins PN-1S, PN-3S, MA-3S, and NPS-609-22, thus prepared, are described. Specimens of glass-reinforced plastics were prepared

Card 1/2

FLIS, I.Ye.[deceased]; TUMANOVA T.A.; GRAD. N.M.; AL'SHITS, I.M.;
DMITRIYEVA, A.N. Prinimatel' uchastiye: GLADKAYA, L.A.; MUDROV,
O.A.; ZUBOVA, G.I.

Effect of water on polyester resins and glass plastics based on
same. Plast.massy no.10:33-36 '64. (MIRA 17:10)

MUDROV, P.

Stand for the sale of ice cream and milk shakes. Sov.torg.
35 no.4:51 Ap '62. (MIRA 15:4)
(Vending stands)

MUDRECV, P.A.

SUBJECT: USSR/Mining Transport Means

127-10-17/24

AUTHORS: Mudrev, P.A. and Serebryanikov, S.I., Engineers

TITLE: Cars for Rock Transport from Open Mines (Vagony dlya otkatki gornoy massy iz kar'yerov)

PERIODICAL: Gornyy Zhurnal, 1957, #10, pp 70-71 (USSR)

ABSTRACT: Most loads from open mines are transported in dump railroad cars. However, in some cases ordinary cars can replace dump cars for transportation of ore and coal to concentration plants.

Dump cars manufactured by the Kaliningrad Plant have a capacity utilization factor of 0.77 for clay ground and 0.88 for rocks. Utilization factors of the dump cars manufactured by the Plant imeni "Pravda" are considerably higher; their values are 0.9 and 1.04 respectively.

According to author's calculations, the optimum capacity of the dump car must be 90 tons when the adhesion weight of electric locomotives is 150 tons. However, with locomotive adhesion weights increased up to 180 to 200 tons, the capacity of dump cars could be increased to 110 to 150 tons .

Card 1/2

MUDROV, Petr Andreyevich; NIKITIN, V. S., doktor tekhn. nauk, prof.,
retsenzent

[Planning and operation of the trackage of railroad
transportation in open-pit mines] Proektirovanie i ekspluata-
tsiia putevogo razvitiia kar'ernogo zheleznodorozhnogo
transporta. Moskva, Nedra, 1965. 160 p. (G. 1. 18:7)

S/194/61/000/007/015/079
D201/D305

AUTHOR: Mudrov, V.I.

TITLE: Problem of evaluating the cancellation of a call in single-channel systems of mixed mass service

PERIODICAL: Referativnyy zhurnal. Avtomatika i radioelektronika, no. 7, 1961, 45, abstract 7 V325 (V sb. Probl. kiber-netiki, no. 4, M., Fizmatgiz, 1960, 45-52)

TEXT: A single-channel system is considered with a fixed service time τ . The call is cancelled if the waiting time exceeds a certain duration. The distribution of intervals between calls is the Poisson distribution. The probability of call cancellation in such a system is easily obtained (a formula has been obtained) if it is seen that the average relative number of unanswered calls tends to probability of call cancellation over a long period of service. The results obtained may be applied to solving problems in servicing users with a "wearing out" instrument. 5 references. [Abstracter's note: Complete translation]

Card 1/1

10.6500

S/044/62/000/002/088/092
C111/C333

AUTHOR: Mudrov, V. I.

TITLE: A queue with "impatient" visitors and variable service time which depends linearly on the time of stay of the visitor in the queue

PERIODICAL: Referativnyy zhurnal, Matematika, no. 2, 1962, 77-78, abstract 2V440. ("Probl. kibernetiki". Vyp. 5. M., Fizmatgiz, 1961, 283-285)

TEXT: Considered is a single-channel system of mass service. The flow of the signal calls is of Poisson type with intensity λ . The waiting time is bounded by a constant τ ; the service time t_s depends on the real waiting time t_w : $t_s = t_{s \max} - at_w$, $a \geq 0$. It is assumed that $\tau \leq t_{s \max} - a\tau = t_{s \min}$. Otherwise, according to the author, the formulas become very complicated. The mean service time

$$\bar{t}_{s \text{ mean}} = t_{s \min} + \frac{1}{\lambda} e^{-\lambda\tau} + a \frac{1}{\lambda} (1 - e^{-\lambda\tau})$$

and the probability of refusal
Card 1/2

✓

A queue with "impatient" visitors ...

S/044/62/000/002/088/092
0111/0333

$$P_{\text{ref}} = 1 - \frac{1}{\lambda t_{s \text{ min}} + e^{-\lambda \tau} + a(1 - e^{-\lambda \tau})}$$

are calculated.

[Abstracter's note: Complete translation.]

Card 2/2

MUDROV, V.I. (Moskva)

Remarks on S.I. Zukhovitskii's article "A problem of
piecewise-linear programming." Zhur. vych. mat. i mat.
fiz. 4 no.5:968-969 S-O '64. (MIRA 17:12)

L 58549-65 EWT(d)/T/ENP(1) Pg-4 IJP(c)

ACCESSION NR: AP5012870

UR/0280/65/000/002/0003/0008

AUTHOR: Mudrov, V. I. (Moscow)

27
B

TITLE: Determining the shortest Hamiltonian paths in a complete graph by the methods of integer programming

SOURCE: AN SSSR. Izvestiya. Tekhnicheskaya kibernetika, no. 2, 1965, 3-8

TOPIC TAGS: Hamiltonian path, complete graph, integer programming

ABSTRACT: A method is presented for obtaining many integer formulations of linear programming which is equivalent to the traveling-salesman problem (Op. Res., v. 11, no. 6, 1964). A complete graph formed by the nodes x_i ($i = 1, 2, \dots, s$) and all a_{ij} branches connecting them is denoted by $[X, A]$. This theorem is proven: The integer with respect to α_j solution of this set:

$$L = \sum_{i=1}^s \sum_{j=1}^s a_{ij} d_{ij} = \min,$$

$$\sum_{j=1}^s a_{ij} = 1, \quad i = 1, 2, \dots, s,$$

Card 1/3

L 58549-65

ACCESSION NR: AP5012870

$$\sum_{j=1}^s a_{ij} = 1, \quad i = 1, 2, \dots, s,$$

$$a_{ij} = \sum_{l=1}^T a_{ij}^l, \quad i, j = 1, 2, \dots, s,$$

$$\sum_{j=1}^s a_{ij}^l = \sum_{k=1}^s \sum_{l=1}^{T-1} k_{ik} a_{kj}^l, \quad i = 1, 2, \dots, s, \quad l = 1, 2, \dots, T-1,$$

$$\sum_{j=1}^s a_{ij}^T = 1,$$

$$a_{ij}^l \geq 0, \quad i, j = 1, 2, \dots, s, \quad l = 1, 2, \dots, T.$$

can serve as a solution of the traveling-salesman problem. Orig. art. has 60 formulas.

Card 2/3

I 58549-65

ACCESSION NR: AP5012870

ASSOCIATION: none

SUBMITTED: 23Jun64

ENCL: 00

SUB CODE: DP

NO REF SOV: 001

OTHER: 002

Card 3/3 *DP*

MUDROV, V.I. (Moskva)

Algorithm for the numeration of combinations. Zhur. vych.
mat. i mat. fiz. 5 no.4:776-778 J1-Ag '65.

(MIRA 18:8)

L 51853-65 EWT(d)/ENP(v)/T/ENP(k)/ENP(h)/ENP(l) Pf-4

ACCESSION NR: AR4046567

S/0271/64/000/008/A019/A019
62.5:658.562

SOURCE: Ref. zh. Avtomat., telemekh. i vychisl. tekhn. Svodnyy tom, Abs. 8A135

AUTHOR: Kovalev, L. P.; Slavinskiy, V. L.; Temnikov, F. Ye.; Mudrov, V. P. 20

TITLE: Equipment of the supervisory center of "Tsentrrotekhnika" system

OUTED SOURCE: Tr. ¹⁴Elek. energ. in-ta, vyp. 52, 1963, 117-123

TOPIC TAGS: industrial automatic control, supervisory control

TRANSLATION: A supervisory (plant-type) center¹⁴ (SC) is intended for collecting and processing production information. Each typical SC benchboard can serve up to 500 control points. A parallel-series method of scanning is used; five groups are scanned simultaneously with a successive scanning of 100 points in each group. Thus, each benchboard covers five plant departments. The SC block diagram comprises the following functional units: a central scanning unit, a sensor switching unit, a parameter-number indicator, a digital display device, a digital recording device, and a deviation-signalling device. The system functions as follows: the central scanning unit feeds to the binary-code-scanning line a periodic sequence of code words; in the time interval between two scanning periods the unit produces pulses

Card 1/2

L 51853-65

ACCESSION NR: AR4046567

for controlling the sensor-switching unit. The latter switches the sensors and also provides addresses for the information by means of the parameter-number indicator. The digital display unit and digital recording unit present, in the decimal form, the information about parameter deviations. Further processing of this information takes place in a central computer into which the information is introduced by a binary code; to form the full value of the parameter in absolute units, the set value, the scale, and the nonlinearity characteristic are also fed to the computer. The deviation signalling device comprises five sections, one for each department, each section having two incandescent lamps with different filters. The deviation upward is signaled by a red light, downward, by green; when the parameter is within its proper limits, no light is visible. The structure and principles of operation of the main units are described in detail. Principal transistorized circuits are given for some typical units. A sketch of the construction of "Tsentrrotekhnika-3" SC unit is shown. Three illustrations.

Bibliography: 1 title.

ENCL: 00

SUB CODE: DP, IE

L.L.
Card 2/2

KARPOV, N.N.; MUDROV, Yu.V.

Antropogen permafrost on the slopes of the southern exposure of the
Kukul'baysk Mountain Range. Vest.Mosk. un. Ser. 5: Geog. 17
no.1:68 Ja-F '62. (MIRA 1047)
(Kukul'baysk Mountains--Frozen ground)

KARPOV, N.N.; MUDROV, Yu.V.

The Quaternary frozen ground on the slope of the southern exposure of
the Kukul'bey Range. Vest. Mosk. un. Ser.5: Geog. 19 no.5:58-59 3-0
'64. (MIRA 18:1)

MUDROVA, A.A.

"To the Methodics of the Isolation of Bacillus Alopecuri Nogt," Dok. An, 25, No. 2,
1939. Mbr. Botanical Lab. Inst of Agri. Gorkiy. -1939-.

ACC NR: AP6035033

(N)

SOURCE CODE: UR/0122/66/000/009/0059/0061

AUTHOR: Fomin, V. V. (Candidate of technical sciences, Docent); ~~Kudrova~~, A. G.
(Engineer)

ORG: none

TITLE: Hydroerosion resistance of titanium coated carbon steel

SOURCE: Vestnik mashinostroyeniya, no. 9, 1966, 59-61

TOPIC TAGS: erosion, titanium, metal diffusion plating

ABSTRACT: The samples were titanium coated at a temperature of 1100-1500°C in a reaction mixture of 15% fluorspar, 4% sodium fluoride, and 81% ferrotitanium, treated with hydrochloric acid. On the surface of the samples there was deposited a layer of the reaction mixture with a thickness of 2-3 mm, and then a layer of ordinary quartz sand with a binder. The duration of the process was 4-6 hours. Increasing the duration of the process did not substantially change the depth and the concentration of the diffusion layer. Increased activity of titanium is attained by previous treatment of the ferrotitanium with hydrochloric acid and by the presence of sodium fluoride in the reaction mixture. X ray analysis of the coating shows that at such a depth of the diffusion layer, the layer consists primarily of a mixture of the solid solution and the chemical compound Fe_2Ti . Hydroerosion tests were made on coatings

Card 1/2

UDC: 620.193.1:669.14'295

ACC NR: AF6035033

prepared in this manner. Metallographic examination of the hydroerosion of the diffusion layer, saturated with titanium, shows that under jet action, there first appear traces of plastic deformation in the form of slip lines and twinning. There then appear at these locations microcracks which grow quickly and turn into failure sites. Failure takes place along the weak grain boundaries as well as in the grains themselves. Nevertheless, the data shows that the titanium coating method described in the article has the advantage of producing a deep diffusion layer with an increased concentration of titanium and rich in carbides, and which has a high degree of hardness. Orig. art. has: 3 figures and 1 table.

SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 003

Card 2/2

L 55115-65 EWT(m)/EWJ(m)/EWP(t)/EWP(b) IJP(a) RDW/JD

ACCESSION NR: AP5016717

UR/026/65/000/010/0019/0019

546,23.24

AUTHOR: Miropol'skaya, N.V.; Rayvich, M.A.; Mudrova, A.I.; Morozov, I.F.; Gerasimov, V.S.

18
B

TITLE: Method of separating selenium and tellurium. Class 12, No. 170921

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 10, 1965, 19

TOPIC TAGS: separation method, selenium, tellurium, selenium separation, tellurium separation, iodine monochloride, iodine monochloride catalyst

ABSTRACT: A method of separating selenium and tellurium by treating solutions containing selenious and tellurous acids with a reducing agent in hydrochloric acid medium with subsequent separation of the precipitated free selenium from the solution. The method is characterized by the fact that in order to increase the purity of the products of separation and increase their yield trivalent arsenic is used as reducer, and the reduction is carried out in the presence of iodine monochloride as catalyst.

[11]

Card 1/2

L 55115-65

ACCESSION NR: AP5016717

ASSOCIATION: none

SUBMITTED: 04Oct62

NO REF BOV: 000

ENCL: 00

OTHER: 000

SUB CODE: IC,GC

ATD PRESS: 4024

Card 2/2

SVOBODA, K., CSc.; MUDROVA, B.

Possibility of preparing radioisotopes in the Czechoslovak
~~cyclotron~~ for use in metallurgy and related fields. Hut
listy 18 no.8:580-583 Ag '63.

1. Ustav jaderného výzkumu, Československá akademie věd,
Rez u Prahy.

TARASEVICH, N.N.; NIKIFOROVA-MENSHUTINA, A.S.; BULK V.F., MUDROVA R.I.

Experience in the preparation of dry agglutinating type-specific
leptospirosis antisera. Zhur.mikrobiol., epid.i immun. 40 no.12:100-
110 D '63. (MIRA 17:12)

1. Iz Moskovskogo instituta vaktsin i syvorotok imeni Mechnikova.

L 53965-65 ENT(m)/EWP(L)/EWP(b) LJP(c) D

ACCESSION NR: AP5013605

UR/0136/65/000/005/0086/0087

669.714

AUTHOR: Marayev, S. Ye.; Mudrova, YeI; Yelina, N. I.

TITLE: Vacuum remelting of electrolytically refined aluminum

SOURCE: Tsvetnyye metally, no. 5, 1965, 86-87

TOPIC TAGS: zone melting, vacuum remelting, high frequency current, aluminum purity, residual electrical resistance, magnesium content, volatile impurity

ABSTRACT: Although electrolytically refined aluminum of the AV0001 and AV0000 types usually has a sufficiently low content of Fe, Cu, and Si impurities, satisfying the GOST All-Union State Standard 3549-55, its magnesium content ($30 \cdot 10^{-4}$ to $50 \cdot 10^{-4}\%$ Mg) is two to three times as high as that of these other impurities. Such an amount of magnesium complicates the zone refining of aluminum. Accordingly, the authors experimented with the elimination of volatile impurities from the melt in a special vacuum melting furnace heated by high frequency current. The effect of the metal before and after the melting on the residual electrical resistance is studied.

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L 53965-65

ACCESSION NR: AP5013605

(p0) at liquid-helium temperature (Fig. 2), as well as from chemical and spectral analyses. Investigations of the composition of ingots melted at 720-740°C in a vacuum (10^{-3} mm Hg) for 1, 2, 4, 8, 16, and 24 hr, showed that the longer the time of vacuum melting is the smaller the content of magnesium becomes and the lower the residual electrical resistance of the aluminum is (Fig. 1). It may be expected that if the aluminum is vacuum-melted for an extremely long time, its residual electrical resistance will approach zero. When ingots of aluminum subjected to vacuum remelting by the method described above are used as the starting material for zone melting, the purity of the final product and the productivity of the zone-melting process increase. Orig. art. has: 2 figures.

ASSOCIATION: none

SUBMITTED: 000

ENCL: 02

SUB CODE: MM

NO REV SOV: 000

OTHER: 000

Card

2/4

L 20644-66 ~~BT(m)/BWA(d)/BWP(t)~~ IJP(e) JD
ACC NR: AP6010305 SOURCE CODE: UR/0136/66/000/003/0077/0079

AUTHOR: Marayev, S. Ye.; Madrova, Ye. I.; Yelina, N. I.

ORG: none

TITLE: Mechanical properties and structure of zone-refined aluminum

SOURCE: Tsvetnyye metally, no. 3, 1966, 77-79

TOPIC TAGS: zone refining, aluminum zone refining, zone refined aluminum, aluminum mechanical property, aluminum structure

ABSTRACT: The mechanical properties and structure of cast and rolled, zone-refined aluminum (ZP) with a total impurity content of $5.4-14.5 \cdot 10^{-4}\%$, and AV0000-grade 99.996%-pure electrolytic aluminum have been investigated. 8.5-kg ingots were cold-rolled into strips 2, 0.5, or 0.05 mm thick and 180 mm wide. Strips 2 and 0.5 mm thick were rolled with kerosene lubricants, and strips 0.05 mm thick were rolled with aviation-gasoline lubricants. As-cast ZP aluminum had a tensile strength of 4.4 kg/mm^2 , a yield strength of 2.7 kg/mm^2 , an elongation of 63.3%, a reduction of area of about 100%, and a Brinell hardness of 14.1 kg/mm^2 . Corresponding figures for AV0000 aluminum were 4.2 kg/mm^2 , 1.9 kg/mm^2 , 46.3%, 87%, and 12.9 kg/mm^2 . The respective strength and elongation of as-rolled ZP aluminum varied, depending on the purity, from 3.2 to 4.0 kg/mm^2 and 1-4% at a thickness of 0.05 mm to $4.5-8.5 \text{ kg/mm}^2$ and 30-45% at a thickness of 2 mm. As-rolled AV0000 aluminum had a higher strength and a much lower

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UDC: 669.715:620.1

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ACC NR: AP6010305

elongation. Annealing of ZP aluminum at temperatures up to 300C had little or no effect on tensile strength; elongation markedly increased only in foil 0.05 mm thick. The tensile strength of rolled AV0000 aluminum dropped sharply and the elongation increased with increasing annealing temperature. ZP aluminum recrystallized completely at temperatures below 20C, while AV0000 aluminum preserved the structure of the cold-rolled metal at temperatures up to 150C. The rapid grain growth in both materials begins at temperatures above 250C. Orig. art. has: 4 figures. [AZ]

SUB CODE: 11, 13/ SUBM DATE: none/ OTH REF: 002/ ATD PRESS: 4126

Card 2/2 BK

NESMEYANOV, An.N.; MUDROVA-YABLONITSKA, V.

Effect of Co^{58} recoil after (γ, n) -reaction in complex compounds
of cobalt: Co(III) triglycinate and vitamin B_{12} . Radiokhimiia
5 no.4:516-519 '63. (MIRA 16:10)

(Cobalt compounds) (Nuclear reactions) (Cyanocobalamin)

Common Elements	Processes and Properties Index	Common Variability Index
1ST AND 2ND ORDERS		1RD AND 4TH ORDERS
<p><i>Fogging of photographic plates by basic dyes.</i> M. Munrović. Phot. Korr. 68, 213-5(1932).—In expts. on the coagulation of a Carey Lea dextrin Ag sol by basic dyes, M. observes no connection between the effectiveness of the dye in this respect and its photographic fogging action. Then, however, the ppt. of dye and Ag is washed by decantation with distilled H₂O 2 or 3 times a day, the supernatant liquid becomes almost colorless after a time with those dyes that fog, whereas it remains more or less strongly colored in the other cases.</p> <p style="text-align: right;">E R Bullock</p>		

BC

Feeling of organic dyes, with special reference to photography. H. Kinnear (A.R. Kinnear, 1908, 7, 76-82). A discussion. R.T.

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100-566 METALLURGICAL LITERATURE CLASSIFICATION

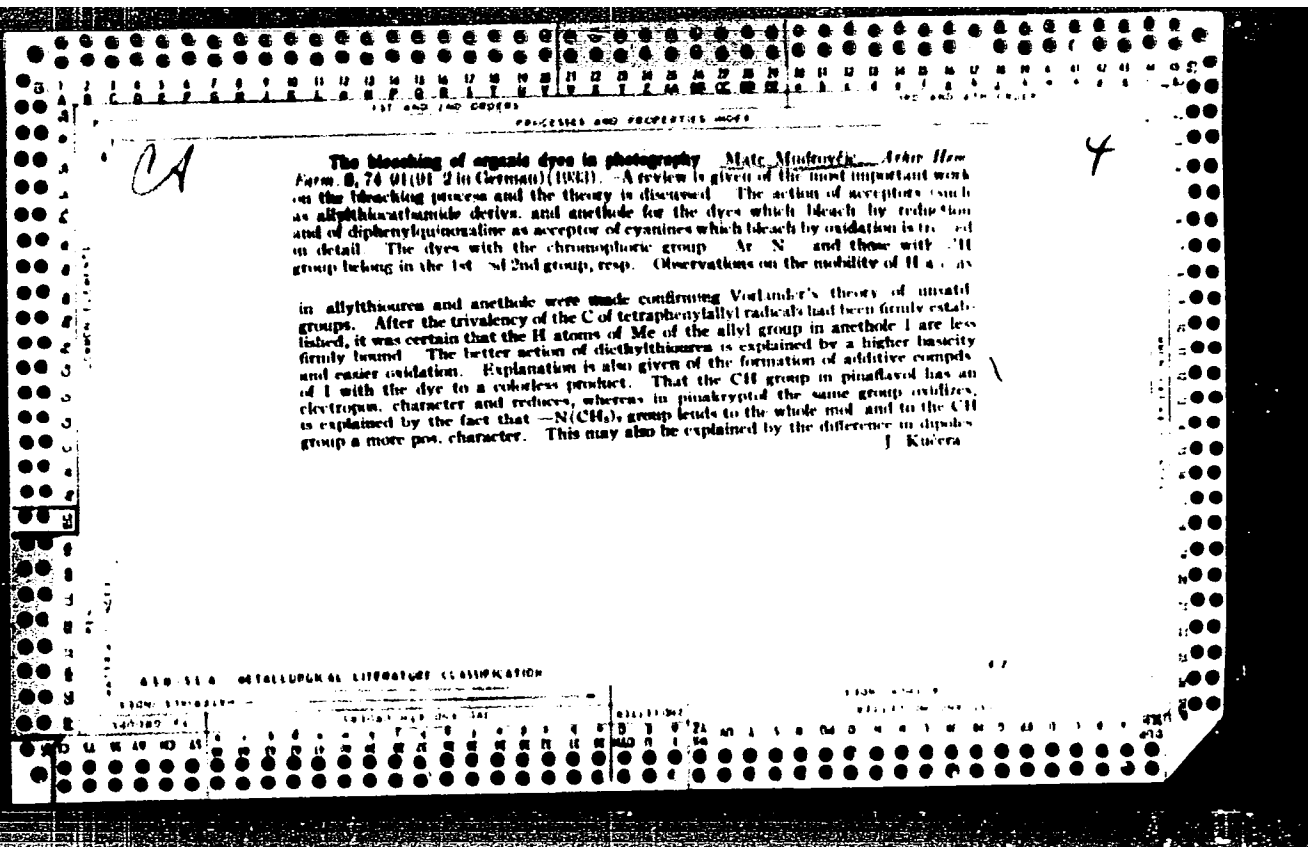
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FROM SYNOPTIC



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Theory of the peroxide reducer. Mate Mudrovic.
 Phil. Rev. 66, 182-4(1933) — The superproportional
 reducing properties of the peroxides are explained by
 certain workers (Scholler, Stenger and Heller) as a catalytic
 phenomenon. Opposed to this theory, L.C. and others
 view the action as best explained by a dispersed theory.
 M. uses colloidal Ag in gelat. in a wide range of concns.
 and the data appear to support the catalytic theory. He
 reconciles previous results. L. B. Muehler

ASS-SEA METALLURGICAL LITERATURE CLASSIFICATION

BOOK DIVISION

SECTION

DATE

BY

REMARKS

CA

The difference between gelatin and collodion silver bromide emulsions, especially as regards desensitizing. Maté Modrovicé. *Phot. Kerr.* 70, 247 (1934). - Expts. on the desensitizing action of methylene blue, phenosafranine, etc., on gelatin and collodion emulsion plates are described. The results indicate that AgBr itself is not capable of being desensitized, that with ripened, undried gelatin emulsions the desensitizing dye acts by destroying (probably by oxidation) the S-contg. sensitizing substances, and that with dye-sensitized gelatin and collodion emulsions the sensitizing dye is either affected chemically or displaced from the grain, by the desensitizing dye. Diethyldithiocarbamide might find practical application for increasing the (blue) sensitivity of collodion AgBr emulsion. E. R. Bullock

COVER
MATERIALS INDEX
COMMON ELEMENTS

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SECTION

REMARKS

1st AND 2ND COVERS																										PROCESSING AND DOCUMENTATION INDEX																										3rd AND 4TH COVERS																									
<p>Photochemical sensitivity of mercuric nitrate. Mata Mudrovic. <i>Bull. soc. chim. roy. Yougoslav.</i> 7, 41-3 (1961) - criticism of the work by Shivic and Nikolic (C. A. 56, 4792) pointing out shortcomings of their inter- pretation of their reactions. The part of the spectrum to which the sensitivity is confined and the difference between discharged and fused conditions of the salt are not sufficiently discussed, it is held. <i>Ibid.</i> 7, 41-3. S. Shivic and D. Nikolic. <i>Ibid.</i> 43-4. - The ultraviolet part of the spectrum trans- mitted by quartz and the sensitivity of a pure salt were discussed in the previous work. References to several authors are made. J. G. Tolpin</p>																																																																													
<p>ASAC SLA METALLURGICAL LITERATURE CLASSIFICATION</p>																																																																													

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Protection of sensitized photographic layers against hal-
tation Mate Murovčić Arhiv Kem 22. 243 55 (1960)
review..... T H James

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"Regeneration of fixing baths and recovery of silver." (To be contd., p. 3).
(KEMIJA U INDUSTRIJI, Vol. 2, no. 4, 1963, Zagreb.)

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August, 1963, Incl.

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"The regeneration of fixing baths and recovery of silver." p. 11. (KEMIJA I
INDUSTRIJA, Vol. 2, no. 3, 1953, Zagreb.)

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August, 1953, incl.

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"Hypersensitivity, Exposure, and Supersensitivity. Fotokemijaka." p. F34.
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Vol. 4, No. 5, May 1955, Uncl.

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YUGOSLAVIA/Physical Chemistry - Radiation Chemistry.

B-10

Photochemistry. Theory of the Photographic Process.

Abs Jour : Ref Zhur - Khimiya, No 8, 1958, 24271

Author : Mudrovcic Mate,

Inst : -

Title : Solarization.

Orig Pub : Kemijska industrija, 1957, 6, No 9, F29-F34.

Abstract : A review.

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